

## Energy Balance in Turbulent Flow

The Reynolds equation is given as

$$\frac{\partial U_i}{\partial t} + U_j \frac{\partial U_i}{\partial x_j} = -\frac{1}{\rho} \frac{\partial P}{\partial x_i} + \nu \frac{\partial^2 U_i}{\partial x_j \partial x_j} - \frac{\partial}{\partial x_j} \overline{u'_i u'_j}. \quad (1)$$

Multiplying (1) by  $U_i$  and rearranging terms, one finds

$$\underbrace{\left[ \frac{\partial}{\partial t} + U_j \frac{\partial}{\partial x_j} \right] \frac{U_i U_i}{2}}_{\text{convection}} = \underbrace{-\frac{\partial}{\partial x_i} \left[ U_i \frac{P}{\rho} + U_j \overline{u'_i u'_j} \right]}_{\text{diffusion by turbulence}} + \underbrace{\nu \frac{\partial^2}{\partial x_j \partial x_j} \frac{U_i U_i}{2}}_{\text{viscous diffusion}} - \underbrace{\nu \frac{\partial U_i}{\partial x_j} \frac{\partial U_i}{\partial x_j}}_{\text{viscous dissipation}} + \underbrace{\overline{u'_i u'_j} \frac{\partial U_i}{\partial x_j}}_{\text{fluctuation energy production}} \quad (2)$$

where

$$\begin{aligned} \left[ \frac{\partial}{\partial t} + U_j \frac{\partial}{\partial x_j} \right] \frac{U_i U_i}{2} &= \text{convection,} \\ -\frac{\partial}{\partial x_i} \left[ U_i \frac{P}{\rho} + U_j \overline{u'_i u'_j} \right] &= \text{diffusion by turbulence,} \\ \nu \frac{\partial^2}{\partial x_j \partial x_j} \frac{U_i U_i}{2} &= \text{viscous diffusion,} \\ \nu \frac{\partial U_i}{\partial x_j} \frac{\partial U_i}{\partial x_j} &= \text{direct viscous dissipation,} \\ \overline{u'_i u'_j} \frac{\partial U_i}{\partial x_j} &= \text{fluctuation energy production.} \end{aligned}$$

Equation (2) is the statement of balance of mean mechanical energy for the mean motion.

Subtracting (1) from the Navier-Stokes equation, it follows that

$$\frac{\partial u'_i}{\partial t} + U_j \frac{\partial u'_i}{\partial x_j} + u'_j \frac{\partial U_i}{\partial x_j} + u'_j \frac{\partial u'_i}{\partial x_j} = -\frac{1}{\rho} \frac{\partial p'}{\partial x_j} + \nu \frac{\partial^2 u'_i}{\partial x_j \partial x_j} + \frac{\partial \overline{u'_i u'_j}}{\partial x_j} \quad (3)$$

Multiplying (3) by  $u'_i$  and taking expected value, we find the equations of balance turbulence energy fluctuation. i.e.,

$$\underbrace{\frac{\partial k}{\partial t} + U_j \frac{\partial k}{\partial x_j}}_{\text{Convection}} = \underbrace{-\overline{u'_i u'_j} \frac{\partial U_i}{\partial x_j}}_{\text{Production}} - \underbrace{\frac{\partial}{\partial x_j} \left[ \frac{\overline{u'_j p'}}{\rho} + \frac{\overline{u'_i u'_i u'_j}}{2} \right]}_{\text{turbulent Diffusion}} + \underbrace{\nu \frac{\partial^2 k}{\partial x_j \partial x_j}}_{\text{Viscous Dissipation}} - \underbrace{\nu \frac{\partial u'_i}{\partial x_j} \frac{\partial u'_i}{\partial x_j}}_{\text{Dissipation}} \quad (4)$$

where  $k = \frac{\overline{u'_i u'_i}}{2}$  is the fluctuation kinetic energy and

$$\frac{\partial k}{\partial t} + U_j \frac{\partial k}{\partial x_j} = \text{convection}$$

$$\overline{u'_i u'_j} \frac{\partial U_i}{\partial x_j} = \text{production}$$

$$\frac{\partial}{\partial x_j} \left[ \frac{\overline{u'_j p'}}{\rho} + \frac{\overline{u'_i u'_i u'_j}}{2} \right] = \text{turbulent diffusion}$$

$$\nu \frac{\partial^2 k}{\partial x_j \partial x_j} = \text{viscous diffusion}$$

$$\nu \frac{\partial u'_i}{\partial x_j} \frac{\partial u'_i}{\partial x_j} = \text{dissipation}$$

## Energy Equation in a Pure Shear Flow

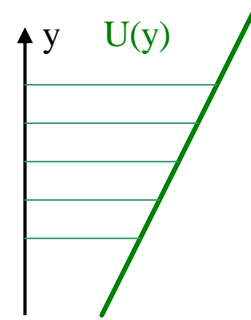
The exact (unclosed) energy equation is given by

$$\frac{D}{Dt} \frac{\overline{u'_i u'_i}}{2} = -\frac{\partial}{\partial x_j} \left[ \overline{u'_j \left( \frac{p'}{\rho} + \frac{u'_i u'_i}{2} \right)} \right] - \overline{u'_i u'_j} \frac{\partial U_i}{\partial x_j} - \varepsilon + \frac{\overline{p' \partial u'_j}}{\rho \partial x_j}$$

Note that the last term is zero.

For a pure shear flow,

$$\mathbf{U} = (U_1(y), 0, 0) \text{ and } \frac{\partial}{\partial x} = \frac{\partial}{\partial z} = \mathbf{U} \cdot \nabla = 0.$$



The energy equation then becomes

$$0 = -\frac{\partial}{\partial y} \left[ \overline{u'_2 \left( \frac{p'}{\rho} + \frac{u'_i u'_i}{2} \right)} \right] - \overline{u'_1 u'_2} \frac{\partial U_1}{\partial y} - \varepsilon + \frac{\overline{p' \partial u'_j}}{\rho \partial x'_j}.$$

The energy equations for  $\frac{1}{2} \overline{u_1'^2}$ ,  $\frac{1}{2} \overline{u_2'^2}$ , and  $\frac{1}{2} \overline{u_3'^2}$  are given as

$$\left( \frac{1}{2} \overline{u_1'^2} \right): \quad 0 = -\frac{\partial}{\partial y} \left( \overline{u'_2 \frac{u'_1 u'_1}{2}} \right) - \overline{u'_1 u'_2} \frac{\partial U_1}{\partial y} - \frac{1}{3} \varepsilon + \frac{\overline{p' \partial u'_1}}{\rho \partial x}$$

$$\left( \frac{1}{2} \overline{u_2'^2} \right): \quad 0 = -\frac{\partial}{\partial y} \left[ \overline{u'_2 \left( \frac{p'}{\rho} + \frac{u'_2 u'_2}{2} \right)} \right] - \frac{1}{3} \varepsilon + \frac{\overline{p' \partial u'_2}}{\rho \partial y}$$

$$\left( \frac{1}{2} \overline{u_3'^2} \right): \quad 0 = -\frac{\partial}{\partial y} \left[ \overline{u'_2 \left( \frac{u'_3 u'_3}{2} \right)} \right] - \frac{1}{3} \varepsilon + \frac{\overline{p' \partial u'_3}}{\rho \partial z}$$

It is observed that the entire production is for  $\frac{\overline{u_1'^2}}{2}$  and there is no direct production of  $\overline{u_2'^2}$  and  $\overline{u_3'^2}$ . Therefore,  $u'_2$  and  $u'_3$  receive their energy from the pressure-velocity interaction terms. That is,  $\overline{p' \frac{\partial u'_2}{\partial y}}$  and  $\overline{p' \frac{\partial u'_3}{\partial z}}$  must be positive and  $\overline{p' \frac{\partial u'_1}{\partial x}}$  must be negative. In most flows,  $\frac{\overline{u_1'^2}}{2}$  is twice as large as  $\frac{\overline{u_2'^2}}{2}$  and  $\overline{u_3'^2}$ .