

Compressible Flows

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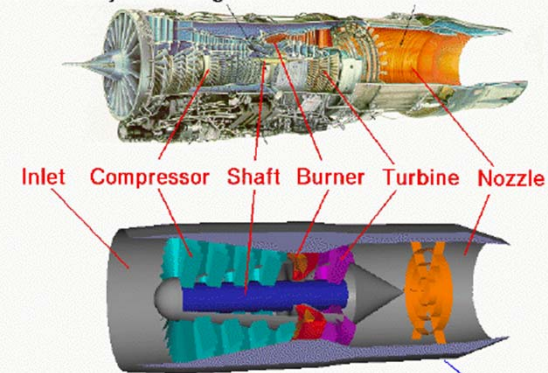
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Pratt & Whitney F100 Engine

Photo



Inlet Compressor Shaft Burner Turbine Nozzle

Simplified Computer Drawing

Outline

- ◆ Compressible Flow Regimes
 - Thermodynamics
 - Speed of Sound & Mach Number
- ◆ Compressible Flows with Area Change
 - Variations with Mach number
- ◆ Shock Waves
 - Nozzle and Diffusers
- ◆ Flows with Friction
- ◆ Flows with Heat Transfer

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Mach Number

$$M = \frac{V}{c}$$

◆ Compressible Flow Regimes

- Incompressible Flow, $M < 0.3$
- Subsonic Flow, $0.3 < M < 0.8$
- Transonic Flow, $0.8 < M < 1.2$
- Supersonic Flow, $1.2 < M < 3$
- Hypersonic Flow, $3 < M$

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Thermodynamics Clarkson University

Enthalpy $h = \hat{u} + P/\rho = \hat{u} + Pv$

Heat Capacity $c_v = \left. \frac{\partial \hat{u}}{\partial T} \right|_v$ $c_p = \left. \frac{\partial h}{\partial T} \right|_p$

First Law $\delta Q = \delta W + d\hat{U}$

First Law (reversible) $TdS = Pd\upsilon + d\hat{u}$
 $TdS = dh - \upsilon dP$

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Idea Gas Clarkson University

Equation of State $\rightarrow P = \rho RT$ $\hat{u} = \hat{u}(T)$

$h = \hat{u} + RT$ $R = \Lambda / M_{\text{gas}}, \Lambda = 8314 \text{ m}^2 / \text{s}^2 \text{K}$

Heat Capacity $c_v = \frac{d\hat{u}}{dT}$ $c_p = \frac{dh}{dT}$

$c_v = \frac{R}{k-1}$ $c_p = \frac{Rk}{k-1}$

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Idea Gas Clarkson University

Gas Constant $R = c_p - c_v$

Air $R_{\text{air}} = 287 \text{ m}^2 / \text{s}^2 \text{K}$ $c_v = 718 \text{ m}^2 / \text{s}^2 \text{K}$
 $c_p = 1005 \text{ m}^2 / \text{s}^2 \text{K}$

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Combined First and Second Laws Clarkson University

$dS = \frac{Pd\upsilon}{T} + \frac{d\hat{u}}{T} = R \frac{d\upsilon}{\upsilon} + c_v \frac{dT}{T}$

$dS = \frac{dh}{T} - \frac{\upsilon dP}{T} = c_p \frac{dT}{T} - R \frac{dP}{P}$

$\rightarrow S_2 - S_1 = c_v \ln\left(\frac{T_2}{T_1}\right) - R \ln\left(\frac{\rho_2}{\rho_1}\right)$

$S_2 - S_1 = c_p \ln\left(\frac{T_2}{T_1}\right) - R \ln\left(\frac{P_2}{P_1}\right)$

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Isoentropic Flows Clarkson University

Pressure Ratio

$$\frac{P_2}{P_1} = \left[\frac{T_2}{T_1} \right]^{k-1} = \left[\frac{\rho_2}{\rho_1} \right]^k$$

Temperature Ratio

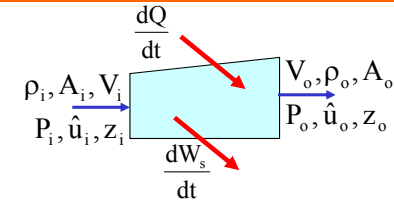
$$\frac{T_2}{T_1} = \left[\frac{P_2}{P_1} \right]^{\frac{k-1}{k}}$$

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Energy Equation Clarkson University

$$\sum \text{Energy Out} = \sum \text{Energy In}$$



$$\frac{dQ}{dt} + \sum_i \dot{m}_i \left(\frac{P_i}{\rho_i} + \hat{u}_i + \frac{V_i^2}{2} + gz_i \right) = \frac{dW_s}{dt} + \sum_o \dot{m}_o \left(\frac{P_o}{\rho_o} + \hat{u}_o + \frac{V_o^2}{2} + gz_o \right)$$

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Energy Equation Clarkson University

Simplified Energy Equation

$$\frac{dQ}{dm} + \left(h_i + \frac{V_i^2}{2} \right) = \left(h_o + \frac{V_o^2}{2} \right)$$

Isoentropic Flows

$$\left(h_i + \frac{V_i^2}{2} \right) = \left(h_o + \frac{V_o^2}{2} \right)$$

Stagnation Enthalpy

$$h_o = \left(h_i + \frac{V_i^2}{2} \right)$$

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Stagnation Properties Clarkson University

Stagnation Temperature

$$c_p T_o = c_p T + \frac{V^2}{2}$$

$$T_o = T + \frac{V^2}{2c_p}$$

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Speed of Sound Clarkson University

Continuity

$$\rho c A = (c - dV)(\rho + d\rho)$$

$$dV = c \frac{d\rho}{\rho}$$

Momentum

$$PA - (P + dP)A = \rho c A (c - dV - c)$$

$$dP = \rho c dV$$

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Speed of Sound Clarkson University

Eliminating dV → $c^2 = \frac{dP}{d\rho} = \left. \frac{\partial P}{\partial \rho} \right|_s$

Speed of Sound → $c^2 = kRT = k \frac{P}{\rho}$

Bulk Modulus → $K = -v \left. \frac{\partial P}{\partial v} \right|_s = \rho \left. \frac{\partial P}{\partial \rho} \right|_s = \rho c^2$

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Concluding Remarks

- ◆ Compressible Flow Regimes
- ◆ Review of Thermodynamics
- ◆ Speed of Sound
- ◆ Mach Number

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Thank you!

Questions?

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