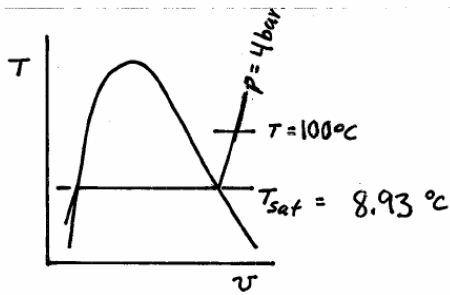


PROBLEM 3.11\*



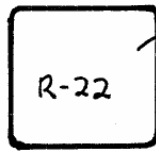
$p = 4 \text{ bar}, T = 100^\circ\text{C}$

Table A-12: superheated vapor

$v = 0.07327 \text{ m}^3/\text{kg}$

$$m = \frac{V}{v} = \frac{(0.1 \text{ m}^3)}{(0.07327 \text{ m}^3/\text{kg})} = 1.36 \text{ kg} \leftarrow m$$

PROBLEM 3.15\*



$V = 1 \text{ m}^3$   
 $p = 1 \text{ bar}$   
 $x = 0.75$

Using data from Table A-8:

$$v = v_f + x(v_g - v_f) = 0.7093 \times 10^{-3} + (0.75)(0.2152 - 0.7093 \times 10^{-3}) = 0.1616 \text{ m}^3/\text{kg}$$

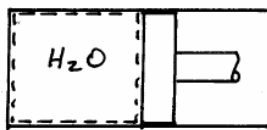
$$m = \frac{V}{v} = \frac{(1 \text{ m}^3)}{(0.1616 \text{ m}^3/\text{kg})} = 6.189 \text{ kg} \leftarrow m$$

PROBLEM 3.34\*

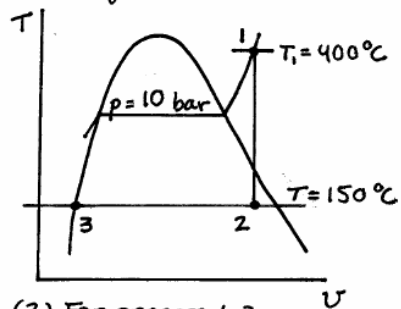
**KNOWN:** Water vapor undergoes a constant volume cooling process followed by isothermal condensation to saturated liquid.

**FIND:** Evaluate the work per unit mass.

**SCHEMATIC & GIVEN DATA:**



$p_1 = 10 \text{ bar}$   
 $T_1 = 400^\circ\text{C}$   
 $T_2 = 150^\circ\text{C}$   
 State 3: sat. liquid at  $150^\circ\text{C}$



**ASSUMPTIONS:** (1) The water is the closed system. (2) For process 1-2, the volume is constant. (3) For process 2-3, the temperature is constant. (4) Volume change is the only work mode.

**ANALYSIS:** By assumptions (2) and (4), only process 2-3 involves work. To evaluate the work, begin with Eq. 2.17

$$W = \int_{v_1}^{v_2} p \, dv \Rightarrow \frac{W}{m} = \int_{v_1}^{v_2} p \, dv$$

Next, we fix each state and obtain relevant data. Since the mass and volume are constant to process 1-2,  $v_2 = v_1$ . From Table A-4;  $v_1 = 0.3066 \text{ m}^3/\text{kg}$ .

With  $v_2 = v_1 = 0.3066$ , we see in Table A-2 at  $150^\circ\text{C}$  that  $v_f < v_2 < v_g$ . Thus, state 2 is in the two-phase, liquid-vapor region. Since the temperature is constant for process 2-3, so is the pressure. That is

$p_2 = p_3 = p_{\text{sat}@150^\circ\text{C}} = 4.758 \text{ bar}$

Finally, from Table A-2,  $v_3 = v_f@150^\circ\text{C} = 1.0905 \times 10^{-3} \text{ m}^3/\text{kg}$ . Thus

$$\frac{W}{m} = \int_{v_1}^{v_2} p dv = p_2 (v_3 - v_2)$$

$$= (4.758 \text{ bar}) (1.0905 \times 10^{-3} - 0.3066) \frac{\text{m}^3}{\text{kg}} \left| \frac{10^5 \text{ N/m}^2}{1 \text{ bar}} \right| \left| \frac{1 \text{ kJ}}{10^3 \text{ N}\cdot\text{m}} \right|$$

$$\textcircled{1} = -145.4 \text{ kJ/kg} \leftarrow \text{W/m}$$

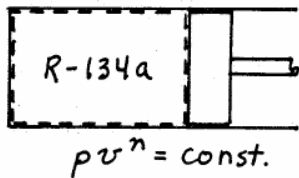
1. The negative sign denotes energy transfer to the system by work during process 2-3.

### PROBLEM 3.53

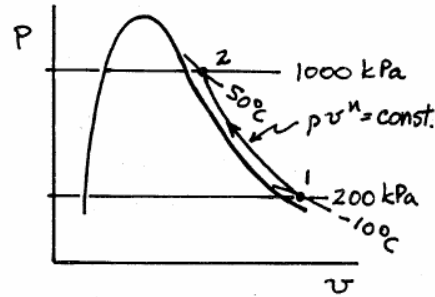
**KNOWN:** Refrigerant 134a undergoes a process for which  $p v^n = \text{constant}$  between two specified states.

**FIND:** Determine the work and heat transfer for the process, each per unit of mass.

**SCHEMATIC & GIVEN DATA:**



$$\begin{aligned} P_1 &= 200 \text{ kPa} \\ T_1 &= -10^\circ\text{C} \\ P_2 &= 1000 \text{ kPa} \\ T_2 &= 50^\circ\text{C} \end{aligned}$$



**ASSUMPTIONS:** 1. The refrigerant is a closed system. 2. The process is described by  $p v^n = \text{constant}$ . 3. Kinetic and potential energy effects are negligible.

**ANALYSIS:** Using Eq. 2.17

$$\begin{aligned} \frac{W}{m} &= \int_{v_1}^{v_2} p dv = \int_{v_1}^{v_2} \frac{\text{const.}}{v^n} dv \\ &= \frac{P_2 v_2 - P_1 v_1}{1-n} \quad (*) \end{aligned}$$

To find the polytropic exponent  $n$ , we first must determine the initial and final specific volumes. Using Table A-12

$$P_1 = 200 \text{ kPa}, T_1 = -10^\circ\text{C} \Rightarrow v_1 = 0.09938 \text{ m}^3/\text{kg}$$

$$P_2 = 1000 \text{ kPa}, T_2 = 50^\circ\text{C} \Rightarrow v_2 = 0.02171 \text{ m}^3/\text{kg}$$

Thus, for the polytropic process

$$P_1 v_1^n = P_2 v_2^n \Rightarrow \log(P_2/P_1) = n \log(v_1/v_2)$$

$$n = \frac{\log(P_2/P_1)}{\log(v_1/v_2)} = \frac{\log(1000/200)}{\log(0.09938/0.02171)} = 1.058$$

Inserting values in Eq. (\*)

$$\begin{aligned} \frac{W}{m} &= \frac{(1000 \text{ kPa})(0.02171 \text{ m}^3/\text{kg}) - (200)(0.09938)}{(1-1.058)} \left| \frac{10^3 \text{ N/m}^2}{1 \text{ kPa}} \right| \left| \frac{1 \text{ kJ}}{10^3 \text{ N}\cdot\text{m}} \right| \\ &= -31.62 \text{ kJ/kg} \leftarrow \text{W/m} \end{aligned}$$

PROBLEM 3.53 (Contd.)

The heat transfer is found by using an energy balance

$$\cancel{\Delta KE} + \cancel{\Delta PE} + \Delta U = Q - W$$

with  $\Delta U = m(u_2 - u_1)$

$$\frac{Q}{m} = (u_2 - u_1) + \frac{W}{m}$$

From Table A-12;  $u_1 = 221.50 \text{ kJ/kg}$  and  $u_2 = 258.48 \text{ kJ/kg}$ . With the result from Problem 3.36 for  $W/m$

$$\frac{Q}{m} = (258.48 - 221.50) + (-31.62 \text{ kJ/kg})$$

$$= +5.36 \text{ kJ/kg} \leftarrow$$

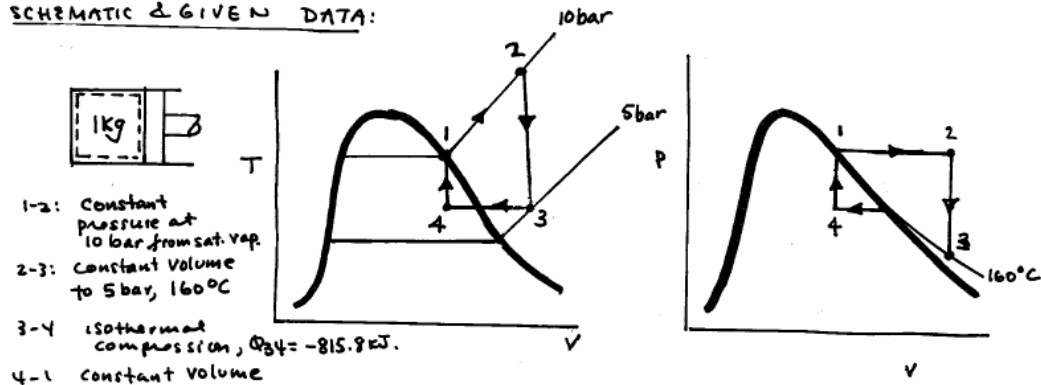
$\frac{Q}{m}$

PROBLEM 3.67

**KNOWN:** One kg of water undergoes a thermodynamic cycle composed of four processes.

**FIND:** Determine the thermal efficiency

**SCHEMATIC & GIVEN DATA:**



**ASSUMPTIONS:** 1. The water is the closed system. 2. Volume change is the only work mode. 3. Kinetic and potential energy effects can be ignored.

**ANALYSIS:** The thermal efficiency of a power cycle is  $\eta = W_{\text{cycle}}/Q_{\text{in}}$  (see discussion of Eqs. 2.42, 43), where  $W_{\text{cycle}} = W_{12} + W_{23} + W_{34} + W_{41}$ .

**Process 1-2:** state 1 is fixed. State 2 is fixed by  $P_2 = 10 \text{ bar}$ ,  $v_2 = v_3$ . From Table A-4

$$v_3 = 0.3835 \frac{\text{m}^3}{\text{kg}}, \quad u_3 = 2575.2 \text{ kJ/kg}$$

$$\Rightarrow W_{12} = \int_1^2 p \, dV = p m (v_2 - v_1) = (10 \text{ bar}) \left| \frac{10^5 \text{ N/m}^2}{1 \text{ bar}} \right| (1 \text{ kg}) (0.3835 - 0.1944) \frac{\text{m}^3}{\text{kg}} \left| \frac{1 \text{ kJ}}{10^3 \text{ N}\cdot\text{m}} \right|$$

$$= 189.1 \text{ kJ}$$

An energy balance reduces to give  $Q = \Delta U + W$ , or

$$Q_{12} = m(u_2 - u_1) + W = (1 \text{ kg}) [3231.8 - 2583.6] + 189.1 \text{ kJ} = 837.3 \text{ kJ}$$

where  $u_2$  is obtained from Table A-3 using  $P_2, v_2 (=v_3)$ .

**Process 2-3:**  $W_{23} = 0$

$$Q_{23} = m(u_3 - u_2) + W_{23} = (1 \text{ kg}) [2575.2 - 3231.8] = -656.6 \text{ kJ}$$

**Process 3-4:**  $Q_{34} = -815.8 \text{ kJ}$  (given). Then,  $\Delta U = Q_{34} - W_{34}$  gives

$$W_{34} = Q_{34} - \Delta U = Q_{34} - m(u_4 - u_3)$$

State 4 is fixed by  $T_4 = 160^\circ\text{C}$ ,  $v_4 = v_1$

$$\therefore x_4 = \frac{v_4 - v_f}{v_g - v_f} = \frac{0.1944 - 1.102/10^3}{0.3071 - 1.102/10^3} = 0.6317$$

$$\Rightarrow u_4 = u_f + x_4(u_g - u_f) = 674.86 + (0.6317)(2568.4 - 674.86) = 1871 \text{ kJ/kg}$$

$$\Rightarrow W_{34} = -815.8 - (1)[1871 - 2575.2] = -111.6 \text{ kJ}$$

Process 4-1:  $W_{41} = 0$ , and

$$\begin{aligned} Q_{41} &= \Delta U + W_{41}^0 = m(u_1 - u_4) \\ &= (1 \text{ kg}) [2583.6 - 1871] \frac{\text{kJ}}{\text{kg}} = 712.6 \text{ kJ} \end{aligned}$$

The net work is then

$$W_{\text{cycle}} = W_{12} + W_{23} + W_{34} + W_{41}$$

$$\textcircled{1} \quad = 189.1 + 0 + (-111.6) + 0 = 77.5 \text{ kJ}$$

To obtain  $Q_{\text{in}}$ ,

$$Q_{\text{in}} = Q_{12} + Q_{41} = 837.3 + 712.6 = 1549.9 \text{ kJ}$$

Then

$$\eta = \left( \frac{77.5}{1549.9} \right) = 0.05 \quad (5\%)$$

---

$\textcircled{1}$  As a check, note that for every cycle  $Q_{\text{cycle}} = W_{\text{cycle}}$ .

$$\begin{aligned} Q_{\text{cycle}} &= Q_{12} + Q_{23} + Q_{34} + Q_{41} \\ &= 837.3 + (-656.6) + (-815.8) + 712.6 = 77.5 \text{ kJ} \end{aligned}$$

which agrees with  $W_{\text{cycle}}$  calculated using the work quantities.