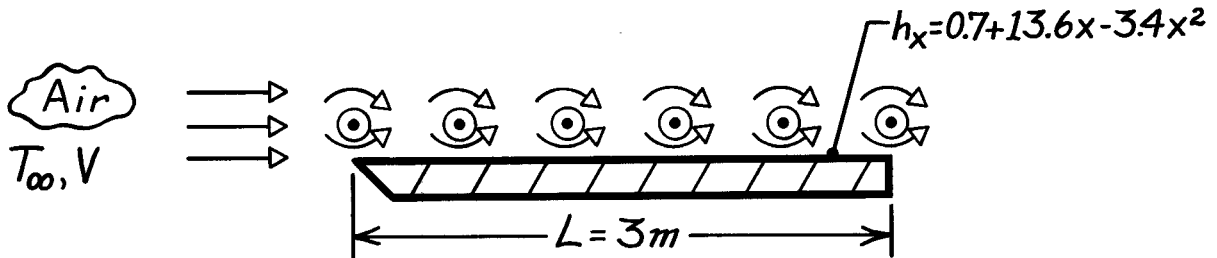


### PROBLEM 6.4

**KNOWN:** Distribution of local convection coefficient for obstructed parallel flow over a flat plate.

**FIND:** Average heat transfer coefficient and ratio of average to local at the trailing edge.

**SCHEMATIC:**



**ANALYSIS:** The average convection coefficient is

$$\bar{h}_L = \frac{1}{L} \int_0^L h_x dx = \frac{1}{L} \int_0^L (0.7 + 13.6x - 3.4x^2) dx$$

$$\bar{h}_L = \frac{1}{L} (0.7L + 6.8L^2 - 1.13L^3) = 0.7 + 6.8L - 1.13L^2$$

$$\bar{h}_L = 0.7 + 6.8(3) - 1.13(9) = 10.9 \text{ W/m}^2 \cdot \text{K.} \quad <$$

The local coefficient at  $x = 3\text{ m}$  is

$$h_L = 0.7 + 13.6(3) - 3.4(9) = 10.9 \text{ W/m}^2 \cdot \text{K.}$$

Hence,

$$\bar{h}_L / h_L = 1.0. \quad <$$

**COMMENTS:** The result  $\bar{h}_L / h_L = 1.0$  is unique to  $x = 3\text{ m}$  and is a consequence of the existence of a maximum for  $h_x(x)$ . The maximum occurs at  $x = 2\text{ m}$ , where

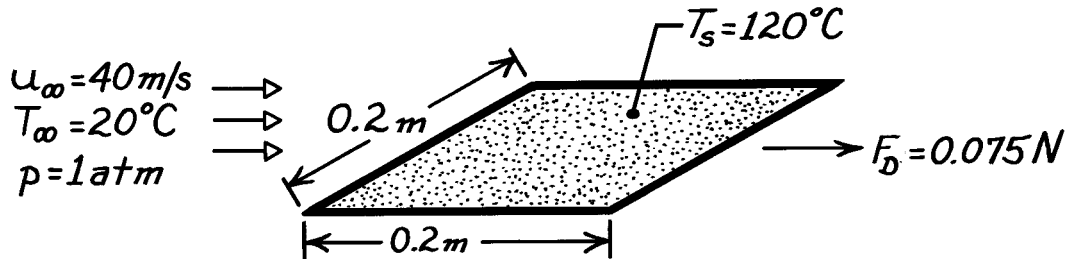
$$(dh_x / dx) = 0 \text{ and } (d^2h_x / dx^2 < 0.)$$

### PROBLEM 6.40

**KNOWN:** Drag force and air flow conditions associated with a flat plate.

**FIND:** Rate of heat transfer from the plate.

**SCHEMATIC:**



**ASSUMPTIONS:** (1) Chilton-Colburn analogy is applicable.

**PROPERTIES:** Table A-4, Air ( $70^\circ\text{C}$ , 1 atm):  $\rho = 1.018 \text{ kg/m}^3$ ,  $c_p = 1009 \text{ J/kg}\cdot\text{K}$ ,  $\text{Pr} = 0.70$ ,  $\nu = 20.22 \times 10^{-6} \text{ m}^2/\text{s}$ .

**ANALYSIS:** The rate of heat transfer from the plate is

$$q = 2\bar{h}(L^2)(T_s - T_\infty)$$

where  $\bar{h}$  may be obtained from the Chilton-Colburn analogy,

$$\begin{aligned} \frac{\bar{h}}{\bar{j}_H} &= \frac{\bar{C}_f}{2} = \bar{\text{St}} \text{Pr}^{2/3} = \frac{\bar{h}}{\rho u_\infty c_p} \text{Pr}^{2/3} \\ \frac{\bar{C}_f}{2} &= \frac{1}{2} \frac{\bar{\tau}_s}{\rho u_\infty^2 / 2} = \frac{1}{2} \frac{(0.075 \text{ N}/2)/(0.2 \text{ m})^2}{1.018 \text{ kg/m}^3 (40 \text{ m/s})^2 / 2} = 5.76 \times 10^{-4}. \end{aligned}$$

Hence,

$$\begin{aligned} \bar{h} &= \frac{C_f}{2} \rho u_\infty c_p \text{Pr}^{-2/3} \\ \bar{h} &= 5.76 \times 10^{-4} (1.018 \text{ kg/m}^3) 40 \text{ m/s} (1009 \text{ J/kg}\cdot\text{K}) (0.70)^{-2/3} \\ \bar{h} &= 30 \text{ W/m}^2 \cdot \text{K}. \end{aligned}$$

The heat rate is

$$q = 2(30 \text{ W/m}^2 \cdot \text{K})(0.2 \text{ m})^2 (120 - 20)^\circ\text{C}$$

$$q = 240 \text{ W}. \quad \leftarrow$$

**COMMENTS:** Although the flow is laminar over the entire surface ( $\text{Re}_L = u_\infty L / \nu = 40 \text{ m/s} \times 0.2 \text{ m} / 20.22 \times 10^{-6} \text{ m}^2/\text{s} = 4.0 \times 10^5$ ), the pressure gradient is zero and the Chilton-Colburn analogy is applicable to *average*, as well as *local*, surface conditions. Note that the only contribution to the drag force is made by the surface shear stress.